

# Optical Wire Guided Lumpectomy

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## ABSTRACT

In practice, complete removal of the tumor during a lumpectomy is difficult to accomplish. Published rates of positive margins, range from 10% to 50%. A spherical lumpectomy specimen with tumor directly in the middle must be obtained more frequently. The proposed optical technique may provide a practical means by which all surgeons may achieve such a resection. It has been shown that the intensity of light sources can be sinusoidally modulated and will predictably become demodulated upon propagation through a scattering medium.

In this work, the modulated light within the medium was collected by optical fiber(s) fixed distance(s) from the source and used to measure the optical properties of the area. The optical properties were then used to calculate the distance the light had traveled through the medium. The fiber was coupled to an 830 nm diode laser that was modulated at 100, 200 and 300 MHz. A handheld optical probe collected the modulated light and a network analyzer measured the phase lag. This data was used to calculate the distance the light traveled from the emitting fiber tip to the probe. An optical phantom as well as a prophylactic mastectomy specimen were used to explore the feasibility of the system.

The optical properties were  $\mu_a = 0.004 \text{ mm}^{-1}$  and  $\mu'_s = 0.38 \text{ mm}^{-1}$  in the phantom. The optical properties for the tissue were  $\mu_a = 0.005 \text{ mm}^{-1}$  and  $\mu'_s = 0.20 \text{ mm}^{-1}$ . The prediction of distance from the source was within 4 mm of the actual distance at 30 mm in the phantom and within 3 mm of the actual distance at 25 mm in the tissue. The feasibility of a frequency domain system that makes measurements of local optical properties then extrapolates those optical properties to make measurements of distance with a separate probe was demonstrated.

keywords: breast cancer, frequency domain, pathlength, distance, *ex vivo* optical properties, lumpectomy

## 1. INTRODUCTION

### 1.1 Lumpectomy for non-palpable tumors is not accurate enough

For small breast cancers and pre-cancerous conditions a lumpectomy, also called breast conserving surgery, is often performed. In this surgical technique, the lesion and surrounding tissue are removed but the remainder of the breast is left intact. Many studies have shown that obtaining negative margins at initial lumpectomy decreases the risk of ipsilateral recurrence and the need for additional surgeries. However, the rate of published negative margins ranges from 50–90%<sup>1–7</sup> and should be improved.

### 1.2 Significance

In the U.S., 200,000 women were diagnosed with breast cancer and another 50,000 were diagnosed with breast cancer *in situ* in 2005; 40,000 women died of the disease.<sup>8</sup> In 2006, 18,000 inpatient lumpectomies occurred<sup>9</sup> and in 1996, the last year the National Survey of Ambulatory Surgery was completed, 341,000 outpatient lumpectomies were performed. The occurrence of breast conserving surgery has increased in the last decade<sup>10–14</sup> so the actual number of procedures performed in 2009 is likely to be higher. It has been demonstrated that lumpectomies followed by breast irradiation have equivalent 12 year ipsilateral recurrence rate as mastectomies for tumors less than 40 mm in diameter with negative or positive axillary lymph nodes.<sup>15,16</sup> However, the margin status of lumpectomies is critical to the success of the treatment. If a margin is positive following lumpectomy, the patient usually undergoes a second surgery to clear the margins. This not only creates additional cost but also prolongs the course of treatment.

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### 1.3 Standard Wire Guided Lumpectomy

More than 25 years ago Daniel Kopans introduced the hookwire technique to simplify the preoperative localization of breast cancers.<sup>17</sup> The hookwire is a 250 mm long thin wire bent at the tip to form a V shaped hook and is now referred to as the Kopans Wire. In practice, a radiologist places a needle in a tumor using either x-ray or ultrasound guidance then slides the Kopans wire, hook end first, through the needle. Once the hook has moved past the end of the needle it springs open in the middle of the tumor and anchors its position. The needle is removed and the wire external to the skin is taped in place to prevent displacement of the wire. Proper placement is confirmed with orthogonal mammograms and the patient is sent to the operating room.

The surgery is guided by the Kopans wire. The surgeon views the mammograms and observes the general location of the tumor and wire. During the operation the wire is followed. Before reaching the end of the wire, the surgeon must deviate from the wire and then re-approach it to excise the tissue surrounding its tip. However, the exact point to deviate from and approach the wire is unclear.

### 1.4 Optical Wire Guided Lumpectomy

It was hypothesized that illuminating the tissue surrounding tumors would result in more successful lumpectomies. Eight patients have been enrolled in a feasibility phase I clinical trial in which the surgery was guided by a light source, a glowball, imbedded in the tumor. The glowball has facilitated a direct surgical approach to the tumor as well as provided a spherically shaped visible guide for resection.

However, it has become clear that light coupling, ambient lighting, eye sensitivity, and the optical properties of breast tissue affect the perceived size of the glowball, and consequently the actual size of the resection. This variability in perceived size can be negated with quantitative measurements of the light exiting the tissue. Adding an intensity modulated light source to the tip of the Kopans wire could allow for intra-operative measurements of the distance from the source to the surgical cutting plane. Using this procedure, optical wire lumpectomies could result in a decrease in positive margins and in more uniform margins. This could result in fewer procedures, reduced cost, and better cosmesis. A system to accomplish this intra-operative measurements is explored in an optical phantom as well as in *ex vivo* breast tissue.

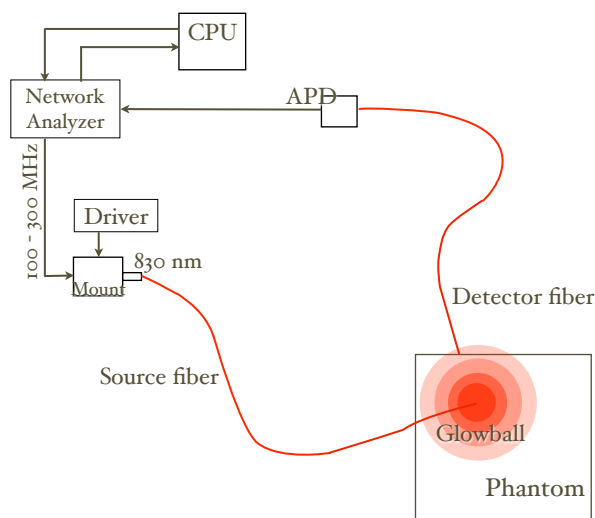


Figure 1. Frequency modulation system.

## 2. MATERIALS & METHODS

### 2.1 Frequency Domain system

To test the feasibility of an experimental measurement to calculate the distance,  $r$ , based on phase measurements, a system was constructed Figure 1. A network analyzer (Hewlett Packard, 8752C) generated a radio frequency (RF) signal of 100, 200, & 300 MHz. The RF signal was delivered to a laser diode mount (ThorLabs, TCLDM9) on which an 830 nm fiber pigtailed laser diode (Sanyo, DL7032-001) was mounted. The laser diode was also driven by a direct current from the driver (ThorLabs, LDC 210). The sinusoidally modulated light was delivered to a phantom through a 200  $\mu\text{m}$  diameter optical fiber and detected with another 1000  $\mu\text{m}$  diameter optical fiber. The detected signal was coupled to an avalanche photodiode, APD, (ThorLabs, APD 210) where it was converted to voltage and fed back into the network analyzer. Calibration of the system was performed by approximating the source and detector fibers to set a phase lag of  $0^\circ$ .

To solve for the optical properties of the medium, unconstrained nonlinear optimization was used in Matlab (Mathworks, v 7.4). Using the mean values of the measured phase at specific distances and modulation frequencies by<sup>18, 19</sup>

$$\theta(r, \omega) = -r \sqrt{\frac{b}{\alpha}} \left(1 + \frac{\omega^2}{b^2}\right)^{1/4} \sin\left(\frac{1}{2} \tan^{-1} \frac{\omega}{b}\right) \quad (1)$$

Where  $c$  is the speed of light in medium,  $b = \mu_a c$ ,  $\alpha = c/3(\mu'_s + \mu_a)$ ,  $\omega = 2\pi f$ ,  $\mu_a$  is the absorption coefficient and  $\mu'_s$  is the reduced scattering coefficient and equals  $\mu_s(1 - g)$  where  $g$  is the anisotropy and  $\mu_s$  is the scattering coefficient. Equation 1 was used to find values of the absorption and reduced scattering coefficients for a limited data set. Then, using the phase measurements at all points and the predicted optical properties of the medium, the distance the light had traveled was calculated by:

$$r = -\frac{\theta}{\sqrt{\frac{b}{\alpha}} \left(1 + \frac{\omega^2}{b^2}\right)^{1/4} \sin\left(\frac{1}{2} \tan^{-1} \frac{\omega}{b}\right)} \quad (2)$$

## 2.2 Polyurethane Phantom

A polyurethane phantom was created. India ink (PRO ART, Beaverton, OR) and titanium dioxide, TiO<sub>2</sub>(Sigma, St. Louis MO) were added to polyurethane components (BJB Enterprises, Inc.), which were then mixed and allowed to cure.<sup>20</sup> Polyurethane was made from two components; component A was unreacted polyurethane and component B was catalyst. India ink was mixed with component A and TiO<sub>2</sub> was mixed with component B. Each component was then placed in a vacuum chamber for degassing, the solutions were held at a reduced pressure until all air bubbles were drawn out of solution. The two components, A:B, were then mixed together in a 100:85 weight ratio respectively. After mixing, the uncured polyurethane was degassed again and then cast into a mold. A cylindrical phantom was cast approximately 60 mm in diameter and 60 mm in height. This served as the tissue simulating phantom. A phantom approximately 60 mm in diameter and 3 mm thick was cast from the same solution; integrating sphere measurements were made on this phantom.

Holes were drilled axially through the cylindrical phantom to half the height of the cylinder as shown in Figure 2A, S indicates the location of the source fiber and  $d_x$  indicates the locations of the detector fiber where  $x$  is the path length between source and detector in mm. Figure 2B is a cross section of the plane at the tip of the fibers. Phase measurements were made within the holes of the phantom at four locations, 10, 20, 30 & 40 mm from the source. The phase was recorded for each distance (i.e. 10 mm was measured then 20 mm, then 30 mm, then 40 mm ) and was repeated 4 times Figure 3 *left*.

The data set used to solve for the optical properties of the phantom held the source-detector separation fixed at  $r = 20$  mm. Measurements of the phase,  $\theta$ , were made at 100, 200 and 300 MHz. Equation 1 was solved with an index of refraction of  $n = 1.468$ .

### 2.2.1 Phantom Characterization

To determine the optical properties of the cured polyurethane, integrating sphere measurements were made of the 3 mm thick phantom. A Xenon light was coupled to a 1 mm diameter fiber and used to make both reflectance and transmittance measurements with an integrating sphere (203.2 mm diameter sphere, 44.5 mm diameter sample

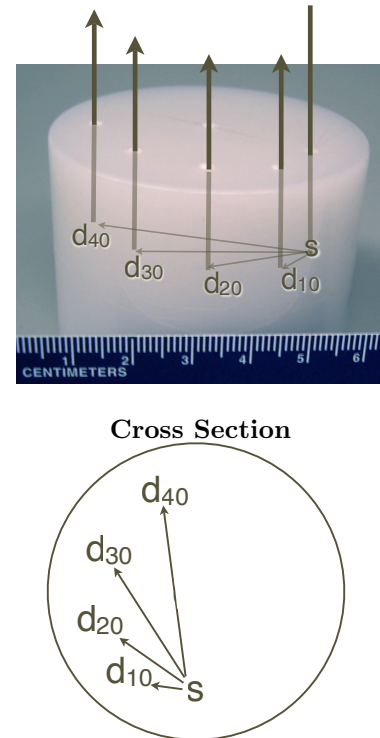


Figure 2. Experimental set up indicating location of source fiber (S) and detector fiber ( $d_x$ ) positions where  $x$  indicates the path length between source and detector in mm. **A.** The polyurethane phantom with fiber locations indicated by thick arrows within the phantom. **B.** Cross section of the phantom in the plane of the fiber tips.

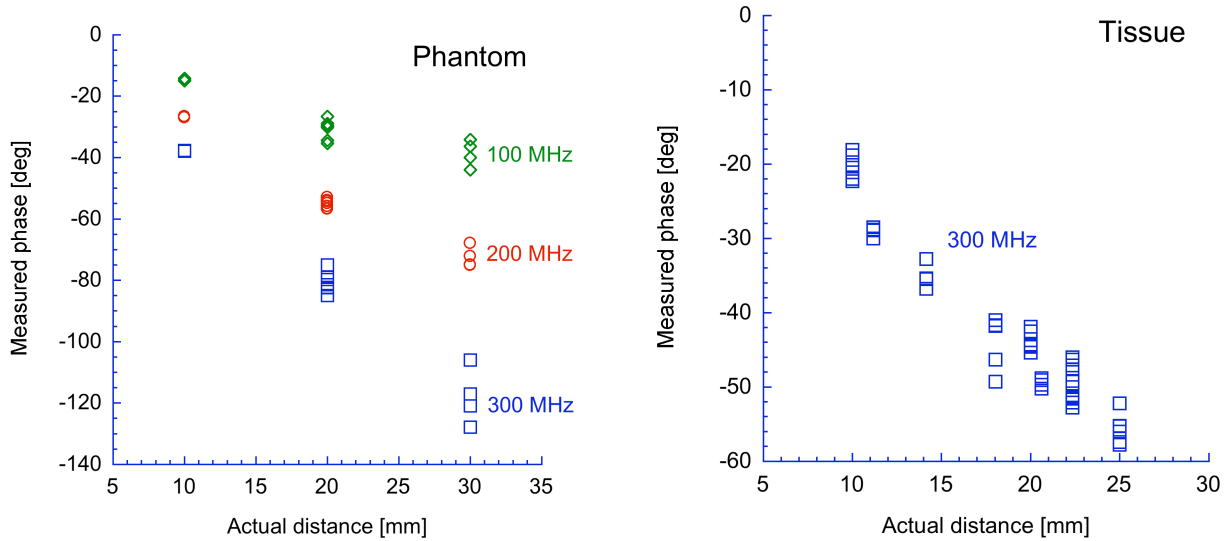


Figure 3. The measured phase as a function of source detector separation distance in the phantom and breast tissue. Squares indicate a modulation frequency of 300 MHz, circles 200 MHz, and diamonds 100 MHz.

port, 6.4 mm entrance port, 0.05 mm diameter illumination beam). The integrating sphere used a 1 mm diameter fiber to couple light into a spectrometer (ISA Horiba) and then a PMT (Products for Research, Inc.) to measure  $M$ . Dark noise,  $M_{dark}$ , and 100%,  $M_{100}$ , signals were measured for reflectance and transmission. A certified reflectance standard (Labsphere) was used for the 100% reflectance measurements. The signal,  $M$  was normalized as follows corresponding to either reflectance,  $R$ , or transmission,  $T$ .

$$R = \frac{M - M_{dark}}{M_{100} - M_{dark}} \quad T = \frac{M' - M'_{dark}}{M'_{100} - M'_{dark}} \quad (3)$$

Three reflectance and three transmission measurements were taken. An inverse adding-doubling method was used to calculate the absorption coefficient,  $\mu_a$ , and the reduced scattering coefficient  $\mu_{s'}$  from the normalized  $R$  and  $T$  measurements.

### 2.3 Tissue Specimen

Following IRB approved protocol, one patient undergoing prophylactic bilateral mastectomy was informed and consented. A cancer-free breast tissue specimen was brought to the lab before pathologic analysis. The specimen had very little skin, approximately 10% of the surface, and was primarily fatty tissue. A needle was inserted diagonally through the tissue from the top to the side far from skin. A 1 mm optical fiber was inserted through the needle and the needle was removed from the tissue. The tip of the optical fiber was in the plane of the side of the tissue and then retracted to a depth of 10 mm. The detector fiber was placed on the surface at 0, 5, 10, 15 and 20 mm from the point of insertion (white dots in Figure 4). The source fiber was then retracted another 10 mm and the measurements repeated. Source detector separation distance was calculated based on the assumption that a  $90^\circ$  angle between the source fiber and the tissue surface existed. Data was collected at 300MHz and a refractive index of 1.38 was used in calculations. Two distances, 10 and 14 mm were used to solve for optical properties using Equation 1. Equation 2 was used to calculate the predicted distance for all other source-detector combinations.

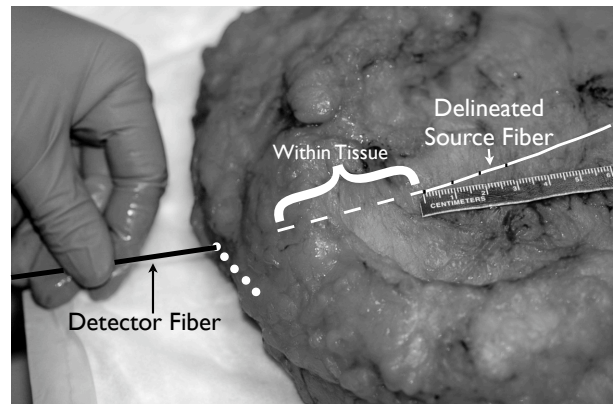


Figure 4. Source and detector positions within the breast tissue.

### 3. RESULTS & DISCUSSION

#### 3.1 Optical Properties

The absorption and reduced scattering coefficients of the polyurethane phantom are given in Figure 5. The optical properties found from integrating sphere measurements were  $\mu_a = 0.003 \pm 0.001(\text{SD}) \text{ mm}^{-1}$   $\mu'_s = 0.41 \pm 0.06(\text{SD}) \text{ mm}^{-1}$  at  $\lambda = 830 \text{ nm}$ . The predicted optical properties from frequency domain measurements were  $\mu_a = 0.004 \text{ mm}^{-1}$  and  $\mu'_s = 0.38 \text{ mm}^{-1}$ . Both methods produced optical properties within one standard deviation of each other.

The optical properties predicted for the tissue were  $\mu_a = 0.005 \text{ mm}^{-1}$  and  $\mu'_s = 0.20 \text{ mm}^{-1}$  which are within the limits of published values for breast tissue.<sup>21–47</sup>

#### 3.2 Phantom Distance Measurements

Figure 6 *top* gives the measured values of phase at 20 mm for 100, 200, & 300 MHz in the phantom as well as the predicted values based on the optical properties that were found to satisfy Equation 1. The distance the light traveled was calculated for the remaining data at 300 MHz and is shown in Figure 7A, where the predicted distance is plotted against the actual distance. Despite the variation in measured optical properties between the integrating sphere & frequency domain techniques, the prediction of distance from the source was within 4 mm of the actual distance of 30 mm in the phantom. Phase measurements were taken at source-detector separation of 40 mm but the signal was not strong enough for reliable measurements and was therefore excluded from analysis. The residuals (actual  $r$  - predicted  $r$ ) are plotted in Figure 7C and range between  $\pm 4 \text{ mm}$ .

#### 3.3 Tissue Distance Measurements

Figure 6 *bottom* gives the measured values of phase at 300 MHz for 10 & 14 mm in the tissue as well as the predicted values based on the optical properties that were found to satisfy Equation 1. The distance the light traveled was calculated for the remaining data at 300 MHz and is shown in Figure 7B, where the predicted distance is plotted against the actual distance. The residuals (actual  $r$  - predicted  $r$ ) are plotted in Figure 7D and also range between  $\pm 4 \text{ mm}$ .

As expected, the residuals increased with distance from the source within the phantom, however the same effect was not seen in the tissue. This could be a result of the changing sampling volume within the tissue, and may have also been confounded by changes in the pressure applied by the detector fiber. Ideally, the device should be able to measure distances of 40–50 mm in any direction from the source and more work is being done to accomplish this goal. Despite a need for improvements in range, the current 4 mm margin of error should be clinically acceptable. The feasibility of using either a two frequency, as in the phantom, or two distance, as in the

	Integrating Sphere [mm <sup>-1</sup> ]	Standard Deviation [mm <sup>-1</sup> ]	Frequency Domain [mm <sup>-1</sup> ]
$\mu_a$	0.003	0.001	0.004
$\mu'_s$	0.41	0.06	0.38

Figure 5. Optical properties of the polyurethane phantom as measured by integrating sphere and frequency domain techniques.

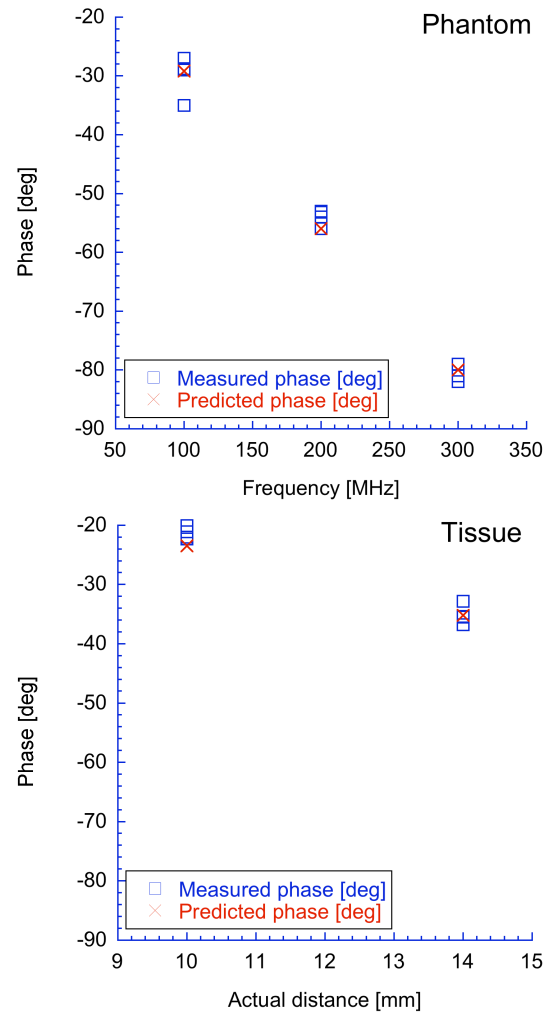


Figure 6. The limited data sets used to solve for the phase in Equation 1. Squares are the measured phase and circles are the predicted values based on the solution to Equation 1

tissue, system to make measurements of local optical properties then extrapolating those optical properties to make a measurement of distance with a separate probe was demonstrated.

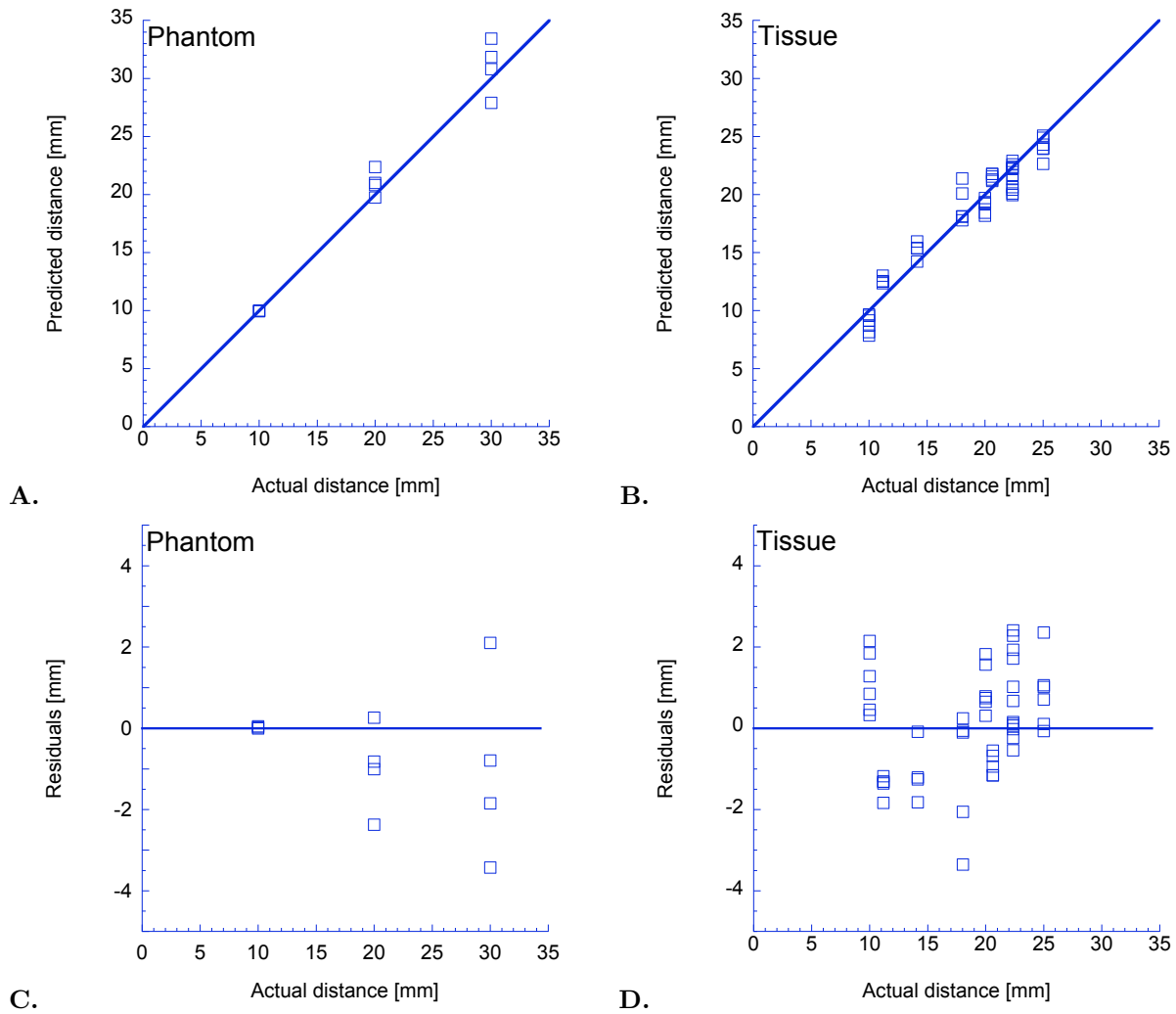


Figure 7. **A.&B.** show the predicted values of distance for each phase measurement. **C.&D.** are the residuals of the difference between the actual distance and the predicted distance.

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